

# Dehydrogenation of propane over a silica-supported vanadium oxide catalyst

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The dehydrogenation of propane over a silica-supported vanadium oxide catalyst was investigated at 823 K under atmospheric pressure in the presence/absence of CO<sub>2</sub>. The yield of propene and the selectivity to propene were higher in the dehydrogenation in the presence of CO<sub>2</sub> than those in the dehydrogenation in the absence of CO<sub>2</sub>. On the other hand, the yield of aromatics and the selectivity to aromatics were much higher in the dehydrogenation in the absence of CO<sub>2</sub> than those in the dehydrogenation in the presence of CO<sub>2</sub>. TPR measurements, NH<sub>3</sub> desorption studies and *in-situ* UV–vis studies on the catalyst were also performed to elucidate the effects of CO<sub>2</sub> on the behavior of the vanadium oxide in the catalyst during the dehydrogenation of propane.

**KEY WORDS:** dehydrogenation; propane; propene; vanadium oxide catalyst; silica.

## 1. Introduction

From environmental points of view, the authors have focused attention on gallium oxide-based catalysts for developing high performance catalysts not containing chromium for the dehydrogenation of propane. The authors recently reported that a silica-supported gallium oxide catalyst was moderately active and highly selective to propene in the dehydrogenation of propane at temperatures ranging from 793 K to 853 K [1,2].

In the present study, the dehydrogenation of propane over a silica-supported vanadium oxide catalyst was investigated. First, the catalytic performance of a silica-supported vanadium oxide catalyst for the dehydrogenation of propane at 823 K was examined in the presence/absence of CO<sub>2</sub>. Then, the reduction of the vanadium oxide catalyst in a stream of H<sub>2</sub> was investigated. NH<sub>3</sub> desorption studies on the acid sites on the catalyst and *in-situ* UV–vis studies on the vanadium species on the catalyst were also performed. Furthermore, the effects of CO<sub>2</sub> on the behavior of the vanadium oxide in the catalyst during the dehydrogenation of propane were discussed on the basis of the experimental findings.

## 2. Experimental

A silica-supported vanadium oxide was prepared by an impregnation method using ammonium vanadate (V). CARI-ACT Q-6 supplied by Fuji Silysia Chemical Ltd. was used for a silica support. An aqueous solution

of ammonium vanadate was added to the silica. Then, the slurry was dried overnight at 383 K, and calcined at 923 K for 2 h. The content of vanadium oxide in the catalyst was 5 wt%. The molar content of vanadium oxide in the catalyst was 1.7 mol%. The surface area of the catalyst was 350 m<sup>2</sup>/g.

The dehydrogenation of propane was carried out using a fixed bed flow reactor. The catalyst fixed in a reactor was treated with a co-feed gas (Ar or CO<sub>2</sub>) before starting the reaction. Then, the dehydrogenation of propane was performed in the presence of Ar or CO<sub>2</sub> under atmospheric pressure at 823 K. The reaction products were analyzed by a FID gas chromatograph and by a TCD gas chromatograph directly connected to the reactor. The products in the dehydrogenation of propane in the absence of CO<sub>2</sub> were H<sub>2</sub>, methane, ethane, ethene, propene, benzene, toluene, trace amounts of other aromatic hydrocarbons, C<sub>4</sub> and C<sub>5</sub> hydrocarbons. In the dehydrogenation in the presence of CO<sub>2</sub>, CO was also formed in addition to the products in the dehydrogenation in the absence of CO<sub>2</sub>. The yield of each product and the selectivity to each product were defined as the conversion of propane to the product and the yield of the product divided by the total conversion of propane, respectively.

The amount of carbonaceous deposits on the post-reaction catalyst was measured by TG/DTA.

Temperature programming reduction (TPR) measurements for the catalyst were carried out using a thermal conductivity detector in a stream of a gas mixture of H<sub>2</sub> (10%) and Ar (90%) in the temperature range from 323 to 923 K under the following operation conditions: 0.1 MPa, flow rate of H<sub>2</sub>/Ar = 20 mL/min, heating rate = 1 K/min. The reduction of the catalyst in

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flowing  $H_2$  at 823 K was also carried using a flow reactor connected to a mass spectrometer (Microvision from Leda-Mass Ltd.). The details of the reduction procedure are described elsewhere [2].

X-ray diffraction (XRD) measurements were also carried out to analyze the phases present in the catalyst. However, only a broad peak assigned to amorphous  $SiO_2$  was detected for the catalyst samples used in the present study, suggesting that vanadium oxide could be highly dispersed on the silica.

In order to characterize the acid sites on the catalyst surface, the desorption of  $NH_3$  pulsed on the catalyst at 823 K was carried out using a pulse reaction apparatus directly connected to the mass spectrometer. The details of the  $NH_3$  desorption procedure are described elsewhere [2].

*In-situ* UV-vis spectroscopic studies on the vanadium species in the catalyst were performed using a UV/VIS/NIR spectrometer (V-570 from JASCO Corp.) equipped with a spectrophotometer and a diffuse reflectance cell supplied from JASCO Corp. The powder sample placed in the cell was treated in a stream of Ar,  $H_2$  or  $CO_2$  at 823 K, and the spectra were taken in the range of 200–800 nm with a reference of  $BaSO_4$  at 603 K, because the spectra taken at higher temperatures were not clear.

### 3. Results and discussion

Figure 1 shows the yields of propene (Yield of  $C_3H_6$ ) and of aromatics such as benzene, toluene and so on (Yield of Arom.), and the selectivities to propene (Sel. to  $C_3H_6$ ) and to aromatics (Sel. to Arom.) in the dehydrogenation of propane in the presence of Ar or  $CO_2$  over a silica-supported vanadium oxide catalyst as a function of time on stream. The yield of propene and the selectivity to propene in the dehydrogenation over the vanadium oxide catalyst in the presence of  $CO_2$  were higher than those in the absence of  $CO_2$ . On the other hand, the yield of aromatics and the selectivity to aromatics in the dehydrogenation over the vanadium oxide catalyst in the presence of  $CO_2$  was much lower than those in the absence of  $CO_2$ . And the conversion of propane in the dehydrogenation in the presence of  $CO_2$  was a little lower than that in the absence of  $CO_2$ . These findings suggest that the dehydrogenation over the vanadium oxide catalyst would be slightly inhibited by  $CO_2$  and that  $CO_2$  would suppress the aromatization of propene to lead to a higher yield of propene and a higher selectivity to propene in the dehydrogenation in the presence of  $CO_2$  than in the dehydrogenation in the absence of  $CO_2$ . In the case of the dehydrogenation in the absence of  $CO_2$ , the pre-treatment of the catalyst with  $H_2$  increased the yield of aromatics and the selectivity to aromatics in the dehydrogenation of propane at 1–3 h of time on stream, whereas it reduced the yield of

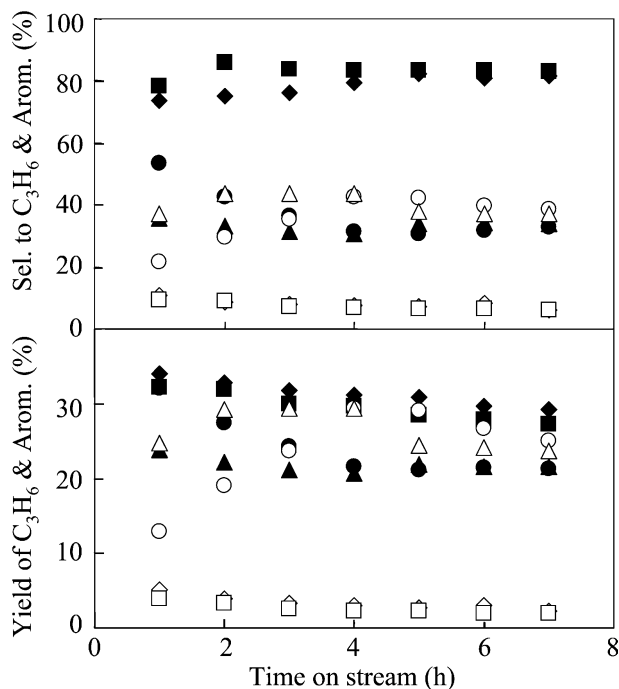


Figure 1. Yields of propene (●, ▲, ■, ◆) and aromatics (○, △, □, ◇), and the selectivities to propene (●, ▲, ■, ◆) and to aromatics (○, △, □, ◇) in the dehydrogenation of propane ( $C_3H_8$ ) over a silica-supported vanadium oxide catalyst not pre-treated (●, ○, ◆, ◇) or over a silica-supported vanadium oxide catalyst pre-treated in  $H_2$  for 2 h (▲, △, ■, □) in the presence of Ar (●, ○, ▲, △) or in the presence of  $CO_2$  (■, □, ◆, ◇) as a function of time on stream. Reaction conditions: 823 K; 0.1 MPa;  $C_3H_8$  concentration in the feed ( $C_3H_8/Ar$ ) = 10%, W/F = 45 g-cat/(mmol- $C_3H_8$ /min).

propene and the selectivity to propene and hardly altered the conversion of propane. In the case of the dehydrogenation in the presence of  $CO_2$ , the pre-treatment of the catalyst with  $H_2$  hardly altered the yields of aromatics and propene and the selectivities to aromatics and to propene in the dehydrogenation. These findings suggest that the pre-treatment of the catalyst with  $H_2$  could increase the number of the acid sites on the catalyst surface. This suggestion could also explain the increase in the yield of aromatics with increasing time on stream during the dehydrogenation in the absence of  $CO_2$  over the catalyst not pre-treated in  $H_2$ . Furthermore, it is also suggested that  $CO_2$  could reduce the number of acid sites on the catalyst surface.

In addition, the dehydrogenation of propane over bulk  $V_2O_5$  in the presence/absence of  $CO_2$  was also carried out. The initial yield of aromatics in the dehydrogenation in the absence of  $CO_2$  was three times higher than that in the dehydrogenation in the presence of  $CO_2$ . The activity of bulk  $V_2O_5$  rapidly decreased with time on stream in the dehydrogenation in the absence of  $CO_2$ , whereas it slowly decreased with time on stream in the dehydrogenation in the presence of  $CO_2$ . These findings suggest that the catalytic properties of vanadium oxide in the silica-supported vanadium oxide catalyst should be almost the same as that of bulk

$V_2O_5$ , and that the acid sites should be formed on vanadium oxide in the catalyst.

The amount of carbonaceous deposits on the catalyst during the dehydrogenation in the presence of  $CO_2$  was much smaller than that during the dehydrogenation in the absence of  $CO_2$ , as shown in figure 2. This finding might be related to the finding described above that the yield of aromatics and the selectivity to aromatics in the dehydrogenation in the presence of  $CO_2$  was much lower than those in the absence of  $CO_2$ . Furthermore, all findings described above suggest that the state of the vanadium oxide in the catalyst in the dehydrogenation in the presence of  $CO_2$  should be much different from that in the dehydrogenation in the absence of  $CO_2$ . Accordingly, the characterization of the vanadium oxide in the catalyst in the presence/absence of  $CO_2$  must be necessary.

TPR measurements for the fresh catalyst and for the catalyst treated with  $CO_2$  after the first TPR measurement, the results of which are shown in figure 3, suggest that vanadium oxide in the catalyst could be reduced at temperatures ranging from 723 to 873 K and that a part of the reduced vanadium oxide in the catalyst could be re-oxidized with  $CO_2$  at 823 K. The peak area for the catalyst treated with  $CO_2$  after the first TPR measurement was about 30% of that for the fresh catalyst. The results of the reduction experiments in a stream of  $H_2$  at 823 K for the fresh catalyst and for the catalyst treated with  $CO_2$  at 823 K after the first reduction are shown in Figure 4. In addition, the oxidation of reduced vanadium oxide in the catalyst with  $CO_2$  was carried out. When a small amount of  $CO_2$  was pulsed at 823 K to the catalyst reduced at 823 K with  $H_2$ , some amount of CO was detected in an effluent gas. These findings strongly supports the suggestion described above.

Desorption measurements of  $NH_3$  pulsed to the catalyst were carried out at 823 K in order to clarify the effects of pre-treatment of the catalyst with  $H_2$  and of re-treatment of the catalyst with  $CO_2$  after the first reduction on the number of the acid sites on the catalyst

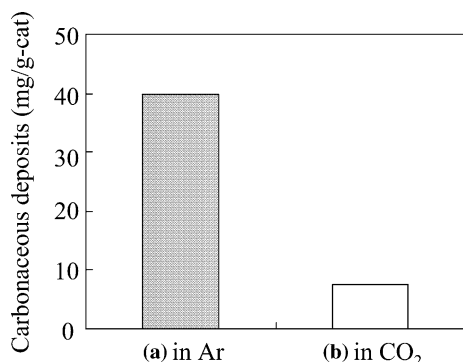


Figure 2. Amount of carbonaceous deposits on a silica-supported vanadium oxide catalyst during the dehydrogenation of propane for 7 h in the presence of Ar (a) or in the presence of  $CO_2$  (b). Reaction conditions were the same as shown in figure 1.

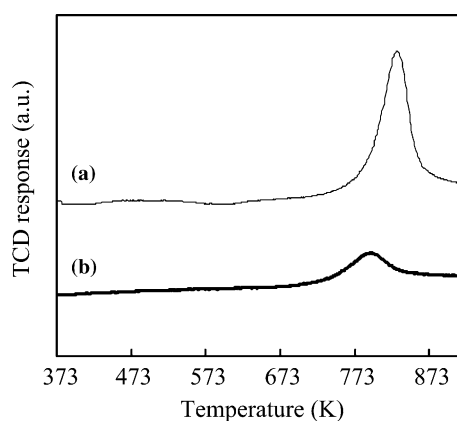


Figure 3. TPR profiles of a fresh silica-supported vanadium oxide catalyst (a) and of a silica-supported vanadium oxide catalyst treated with  $CO_2$  at 823 K for 1 h after the first reduction (b) in a stream of a gas mixture of  $H_2$  (10%) and Ar (90%) in the temperature range from 323 to 923 K. Operation conditions: 0.1 MPa;  $H_2/Ar = 1/9$ ; flow rate of  $H_2/Ar = 20$  mL/min; heating rate = 10 K/min.

at the temperature of the dehydrogenation. The results of the measurements are shown in figure 5. The pre-treatment of the catalyst with  $H_2$  at 823 K increased the retention time of  $NH_3$  on the vanadium oxide catalyst. This finding strongly supports the suggestion previously described that the pre-treatment of the vanadium oxide catalyst with  $H_2$  could increase the number of acid sites on the catalyst. On the other hand, the retention time of  $NH_3$  on the catalyst re-treated with  $CO_2$  after the first reduction was almost the same as that on the catalyst treated in Ar, suggesting that  $CO_2$  could reduce the

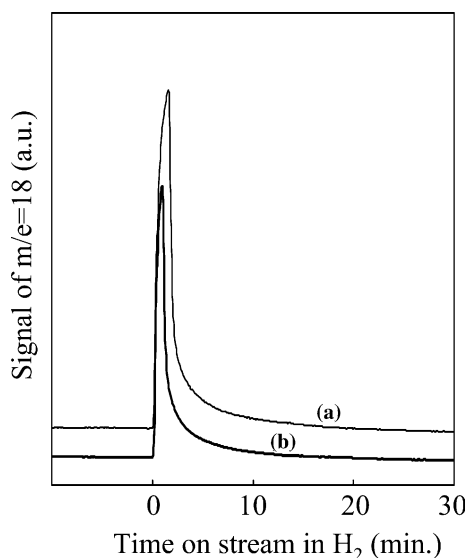


Figure 4. A signal of  $m/e = 18$  as a function of time on stream in  $H_2$  during the reduction of a fresh silica-supported vanadium oxide catalyst (a) or of a silica-supported vanadium oxide catalyst treated with  $CO_2$  at 823 K for 1 h after the first reduction (b) at 823 K after raising the catalyst temperature up to 823 K in a stream of He. Operating conditions: 0.1 MPa; the flow rate of  $H_2$  (He) = 60 ml/min; the weight of sample = 0.2 g.

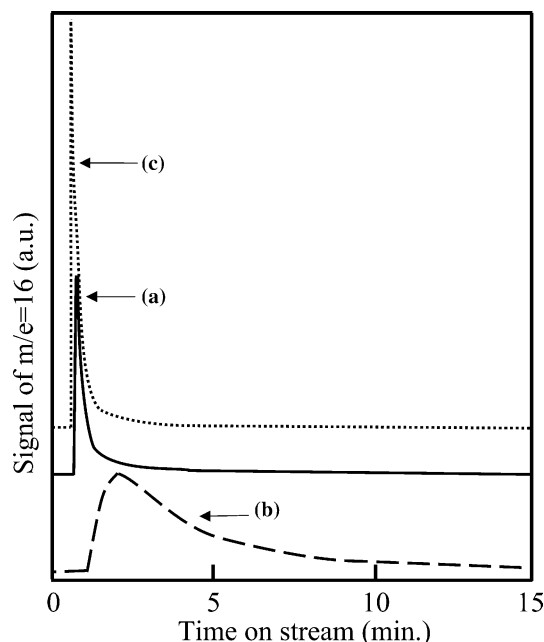


Figure 5. A signal of  $m/e = 16$  in the effluent gas after a small amount of  $\text{NH}_3$  was pulsed at 823 K over the vanadium oxide catalyst pre-treated in Ar at 823 K for 1 h (a), the vanadium oxide catalyst pre-treated in  $\text{H}_2$  at 823 K for 2 h (b) or the vanadium oxide catalyst treated with  $\text{CO}_2$  at 823 K for 1 h after the first pre-treatment in  $\text{H}_2$  at 823 K for 2 h (c) as a function of time on stream in Ar (a, c) or in  $\text{H}_2$  (b). Operating conditions: 0.1 MPa; temperature of the sample = 823 K; flow rate of Ar or  $\text{H}_2 = 20$  ml/min;  $\text{NH}_3/\text{Ar} = 1/9$  (mol/mol).

number of the acid sites on the catalyst, as previously described.

Figure 6 shows *in situ* UV–vis spectra of the catalyst treated at 823 K under various gas compositions. In the

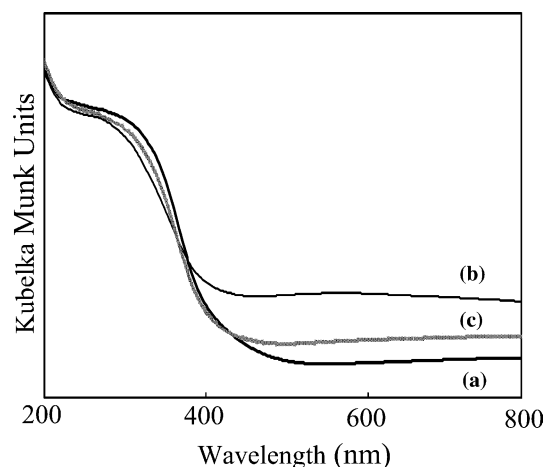


Figure 6. *In-situ* UV–vis diffuse reflectance spectrum at 603 K of the vanadium oxide catalyst pre-treated in Ar at 823 K for 1 h (a), the vanadium oxide catalyst pre-treated in  $\text{H}_2/\text{Ar}$  at 823 K for 2 h (b) or the vanadium oxide catalyst treated with  $\text{CO}_2$  at 823 K for 1 h after the first pre-treatment in  $\text{H}_2$  at 823 K for 2 h (c). Operation conditions: 0.1 MPa; 603 K; flow rate of Ar,  $\text{H}_2/\text{Ar}$  or  $\text{CO}_2 = 60$  ml/min;  $\text{H}_2/\text{Ar} = 1/9$  (mol/mol).

case of the catalyst treated at 823 K in Ar, UV–vis absorption bands located below 400 nm, which should be assigned to the oxygen ligand to metal charge transfer bands of  $\text{V}^{5+}$  [3,4], were observed. On the other hand, in the case of the catalyst treated at 823 K in  $\text{H}_2/\text{Ar}$ , a UV–vis absorption bands above 400 nm, which should be assigned to a weak d-d transition of  $\text{V}^{4+}/\text{V}^{3+}$  [3], were observed and UV–vis absorption bands below 400 nm decreased. In the case of the catalyst treated at 823 K with  $\text{CO}_2$  after the first reduction, UV–vis absorption bands below 400 nm increased and UV–vis absorption bands above 400 nm decreased. These findings suggest that the vanadium on the surface of vanadium oxide in the catalyst could be  $\text{V}^{4+}/\text{V}^{3+}$  in  $\text{H}_2$  and in the dehydrogenation in the absence of  $\text{CO}_2$ , whereas that could be  $\text{V}^{5+}$  in the dehydrogenation in the presence of  $\text{CO}_2$  by the oxidizing action of  $\text{CO}_2$ .

Although DRIFTS measurements on the catalyst were made in order to obtain some useful information about acid sites on reduced vanadium oxide in the catalyst, the band which should be assigned to O–H bond of V–O–H could not be clearly detected owing mainly to the overlapping with O–H bond of Si–OH groups. However, the experimental findings in the present study are very similar to those in our previous study on the dehydrogenation of propane over a silica-supported gallium oxide catalyst. Accordingly, it is suggested that the acid sites on vanadium oxide would be V–O–H sites adjacent to  $\text{V}^{4+}/\text{V}^{3+}$  sites like Ga–O–H sites adjacent to  $\text{Ga}^\delta$  sites which was suggested in our previous study [2].

In summary, the findings in the present study suggest that the vanadium in the silica-supported vanadium oxide catalyst could be reduced to  $\text{V}^{4+}/\text{V}^{3+}$  in the dehydrogenation of propane in the absence of  $\text{CO}_2$  to lead to the formation of acid sites on the surface of the vanadium oxide. The acid sites formed could produce a higher yield of aromatics and a larger amount of carbonaceous deposits. The present findings also suggest that the vanadium on the surface of vanadium oxide in the dehydrogenation of propane in the presence of  $\text{CO}_2$  could be  $\text{V}^{5+}$  which could not lead to the formation of acid sites but result in a higher yield of propene and a smaller amount of carbonaceous deposits.

#### 4. Conclusions

1. The dehydrogenation of propane over a silica-supported vanadium oxide catalyst was investigated at 823 K in the presence/absence of  $\text{CO}_2$ . The yield of propene and the selectivity to propene were higher in the dehydrogenation in the presence of  $\text{CO}_2$  than those in the dehydrogenation in the absence of  $\text{CO}_2$ . On the other hand, the yield of aromatics and the selectivity to aromatics were much higher in the dehydrogenation in the absence of  $\text{CO}_2$  than those in the dehydrogenation in the presence of  $\text{CO}_2$ . In

addition, the amount of carbonaceous deposits on the catalyst during the dehydrogenation in the presence of  $\text{CO}_2$  was smaller than that during the dehydrogenation in the absence of  $\text{CO}_2$ .

2. The vanadium oxide in the catalyst could be reduced at temperatures ranging from 723 to 873 K and a part of the reduced vanadium oxide in the catalyst could be re-oxidized with  $\text{CO}_2$  at 823 K.
3.  $\text{NH}_3$  desorption studies on the vanadium oxide catalyst suggest that the pre-treatment of the vanadium oxide catalyst with  $\text{H}_2$  could increase the number of acid sites on the catalyst and that  $\text{CO}_2$  could reduce the number of the acid sites on the catalyst.
4. UV-vis studies on the vanadium oxide in the catalyst suggest that the vanadium on the surface of vanadium oxide in the catalyst could be  $\text{V}^{4+}/\text{V}^{3+}$  in  $\text{H}_2$  and in the dehydrogenation in the absence of  $\text{CO}_2$ , whereas that could be  $\text{V}^{5+}$  in the dehydrogenation in the presence of  $\text{CO}_2$  by the oxidizing action of  $\text{CO}_2$ .
5. The findings in the present study suggest that the vanadium in the silica-supported vanadium oxide

catalyst could be reduced to  $\text{V}^{4+}/\text{V}^{3+}$  in the dehydrogenation of propane in the absence of  $\text{CO}_2$  to lead to the formation of acid sites on the surface of the vanadium oxide. The acid sites formed could produce a higher yield of aromatics and a larger amount of carbonaceous deposits. It is also suggested that the vanadium on the surface of vanadium oxide in the dehydrogenation of propane in the presence of  $\text{CO}_2$  could be  $\text{V}^{5+}$  which could not lead to the formation of acid sites but result in a higher yield of propene and a smaller amount of carbonaceous deposits.

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